

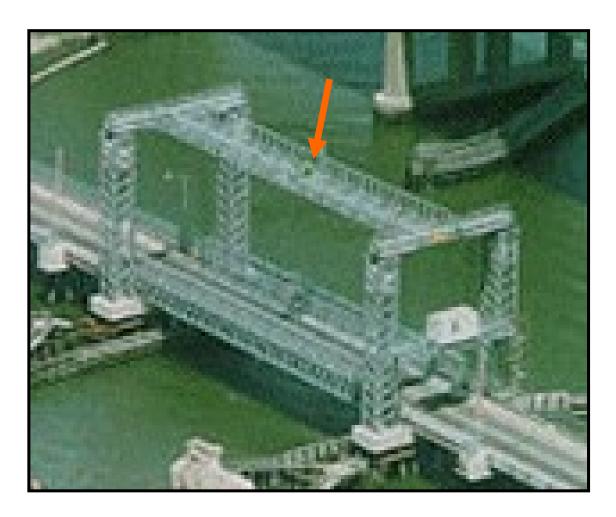
SCOTT SNELLING, EIT

## OUTLINE

- o ANATOMY
- o ALIGNMENT OF COMPONENTS
- o DEFLECTIONS
- o SPAN ALIGNMENT
- o ROPE LAY & CWT. TWIST



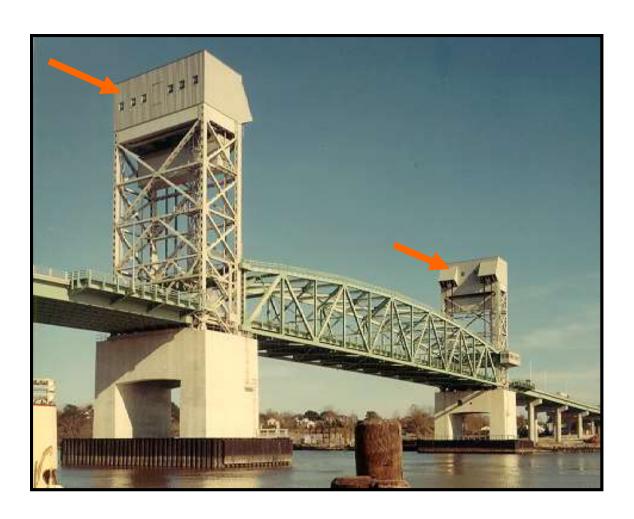
HALSTEAD STREET, CHICAGO



TOWER SPAN DRIVE

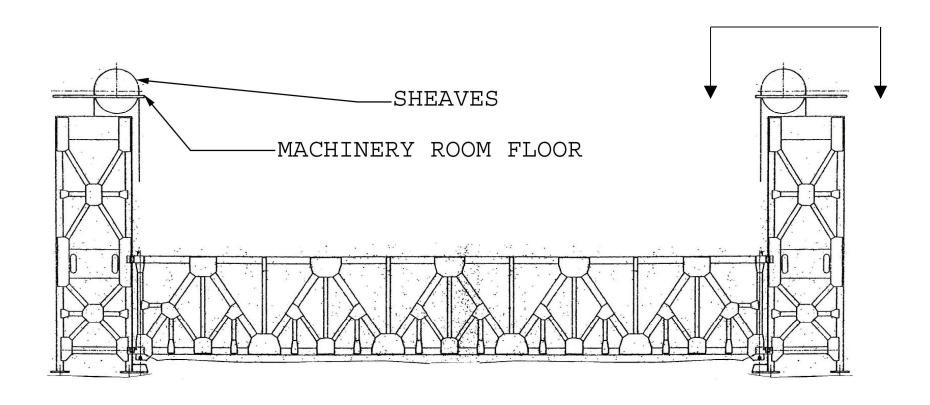


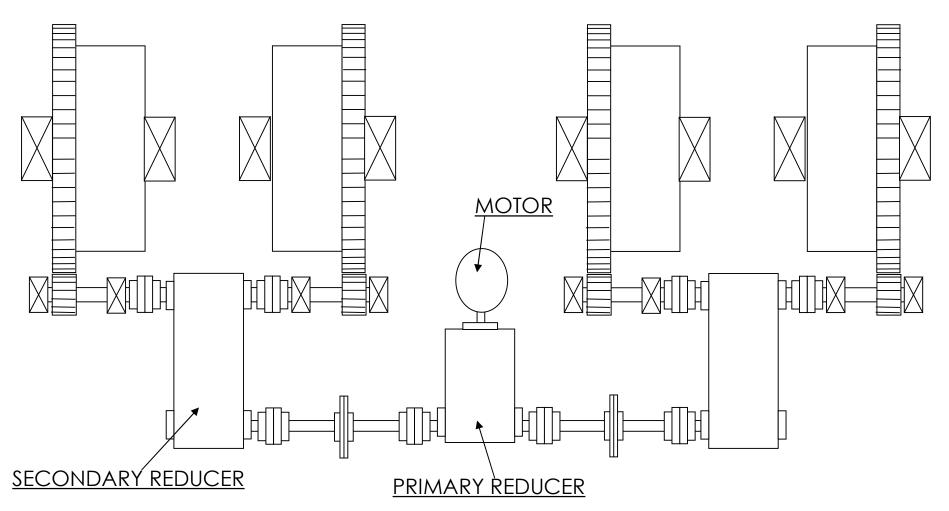
SPAN DRIVE



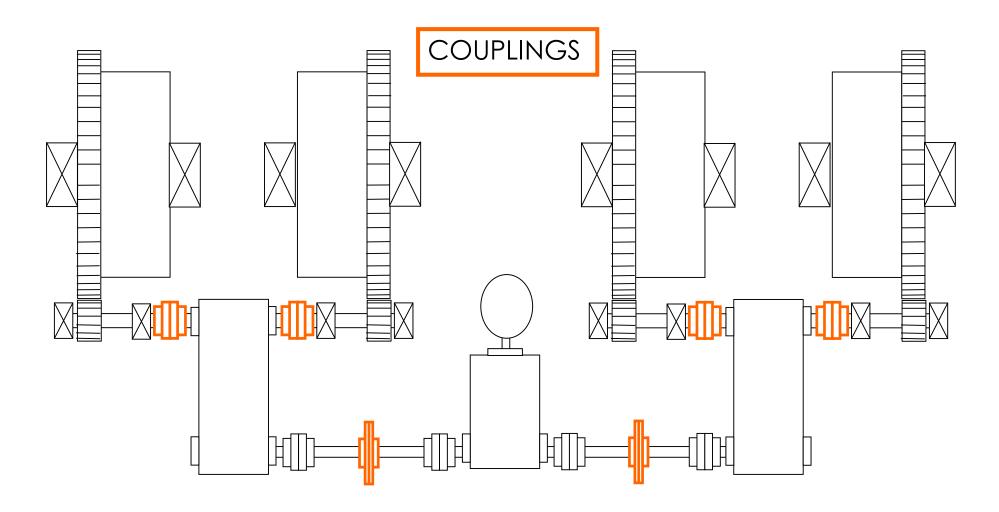
TOWER DRIVE

# ANATOMY OF TOWER DRIVE VERTICAL LIFT BRIDGES

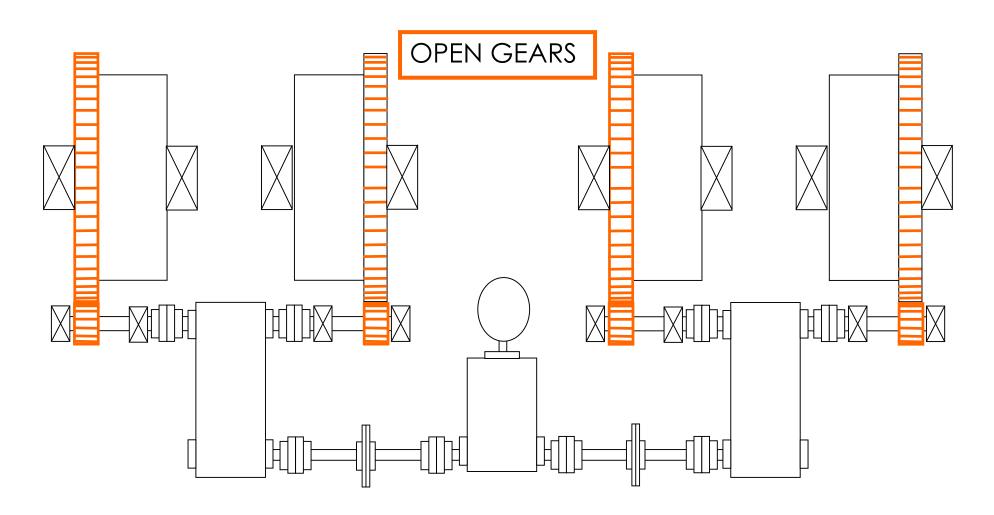




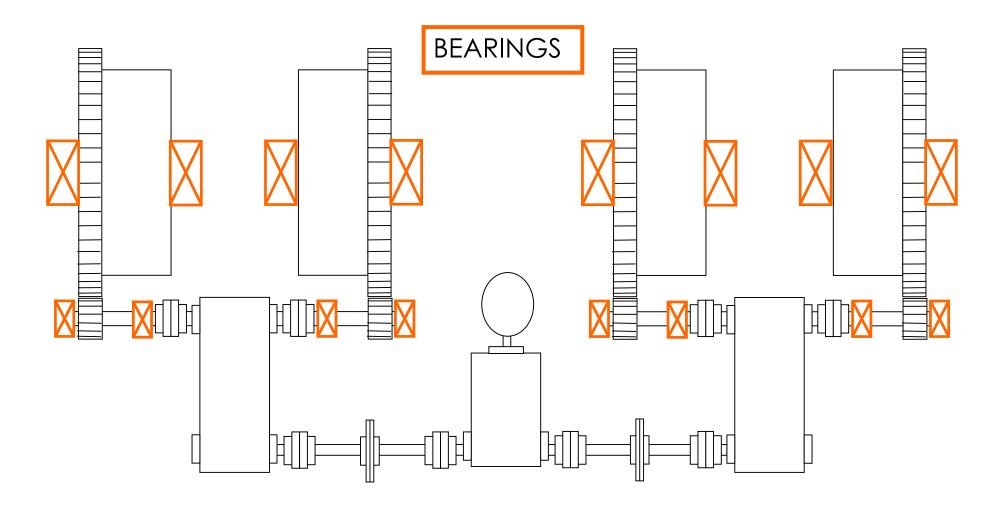
SAMPLE MACHINERY ROOM PLAN



#### SAMPLE MACHINERY ROOM PLAN



### SAMPLE MACHINERY ROOM PLAN



### SAMPLE MACHINERY ROOM PLAN

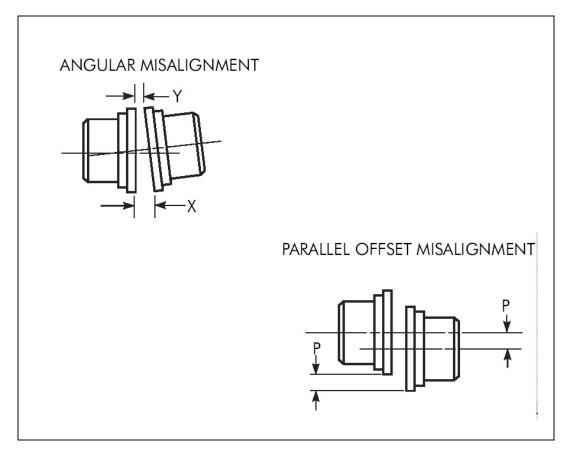
# OUTLINE

- o ANATOMY
- ALIGNMENT OF COMPONENTS
- o DEFLECTIONS
- o SPAN ALIGNMENT
- o ROPE LAY & CWT. TWIST

COUPLINGS

o GEARING

o BEARINGS



o COUPLINGS

**GEARING** 

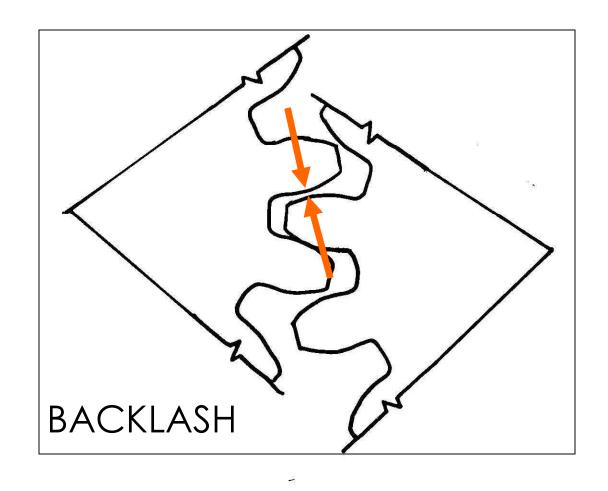
o BEARINGS



o COUPLINGS

GEARING

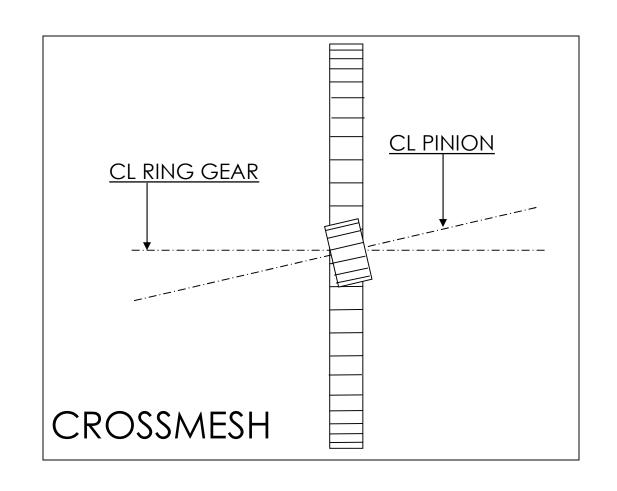
o BEARINGS



o COUPLINGS

**GEARING** 

o BEARINGS



o COUPLINGS

o GEARING

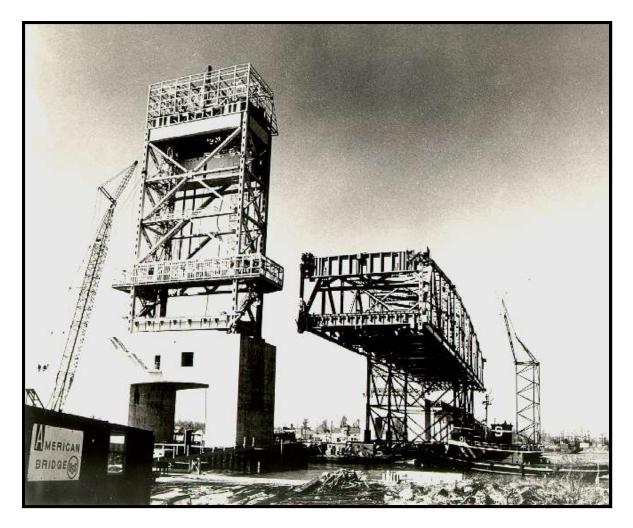
**BEARINGS** 



### OUTLINE

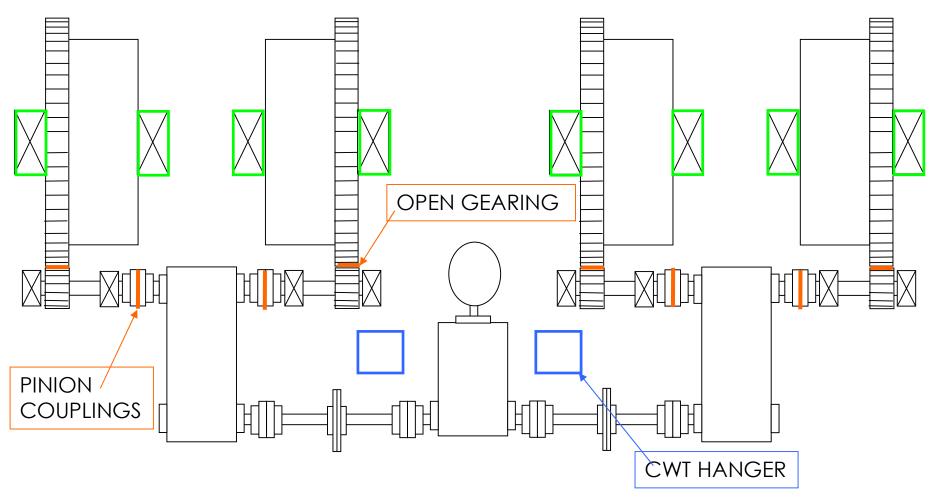
- o ANATOMY
- o ALIGNMENT OF COMPONENTS
- DEFLECTIONS
- o SPAN ALIGNMENT
- o ROPE LAY & CWT. TWIST

### MISALIGNMENTS DUE TO DEFLECTIONS



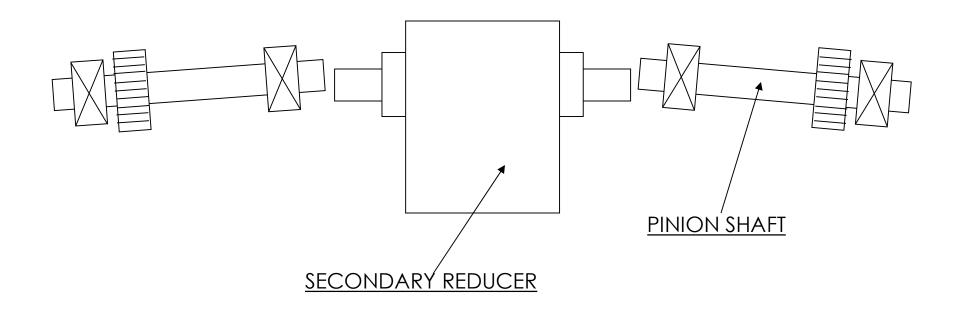
CAUSE OF DEFLECTIONS

### MISALIGNMENTS DUE TO DEFLECTIONS



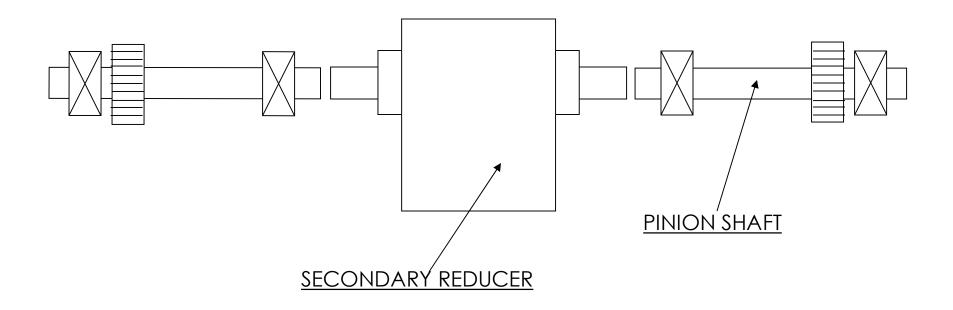
EFFECTED MACHINERY COMPONENTS

# EFFECT OF DEFLECTIONS ON PINION COUPLING



#### **ELEVATION**

# EFFECT OF DEFLECTIONS ON PINION COUPLING



#### **ELEVATION**

### EFFECT OF DEFLECTIONS ON BACKLASH

	East Tower			→ North				
Sheave Number	4		3		2		1	
Side of Tooth	S	N	S	N	S	N	S	N
Tuesday No Load on Sheaves	95	110	124	116	79	80	125	110
Wednesday Load on Sheaves	48	60	139	119	152	155	104	88
Change Due to Deflections	-47.00 tigh	-50.00	15.00 loo:	3.00	73.00	75.00 ser	-21.00 tigh	-22.00 nter

<sup>\*</sup> All Measurements in thousandths of an inch - The specifications called for a backlash of 90 plus or minus 10.

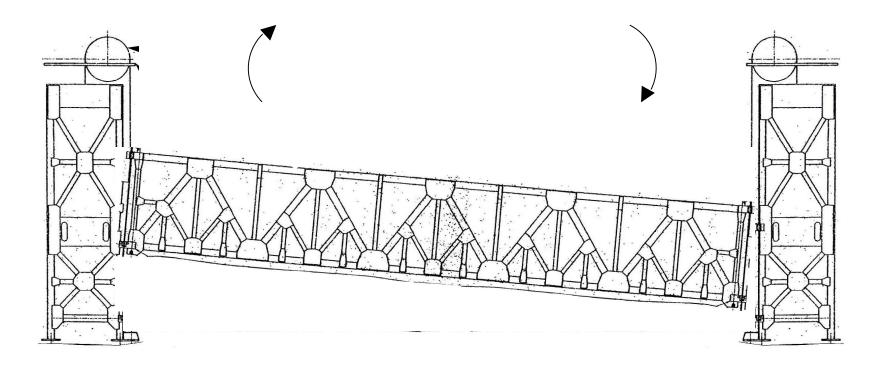
## OUTLINE

- o ANATOMY
- o ALIGNMENT OF COMPONENTS
- o DEFLECTIONS
- SPAN ALIGNMENT
- o ROPE LAY & CWT. TWIST

### ADJUSTING SPAN ALIGNMENT

### SKEW

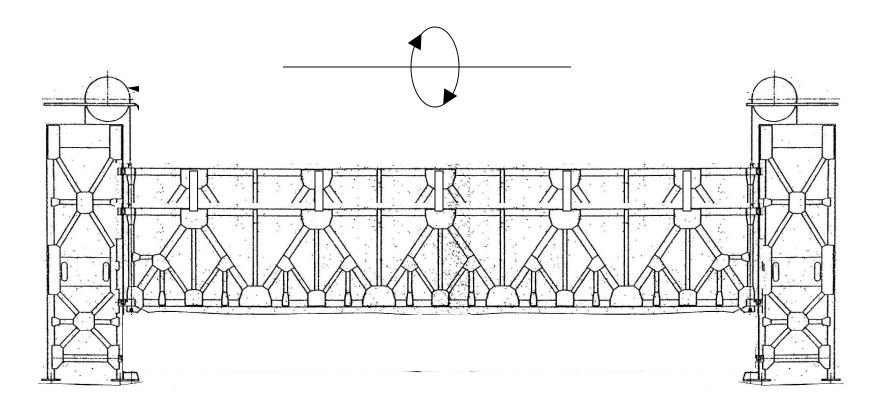
o WARP



### ADJUSTING SPAN ALIGNMENT

o SKEW

### WARP



### GOALS OF SPAN ADJUSTMENT

- o SHEAVES DRIVEN WITH EQUAL POWER
- o LIVE LOAD SHOES WITH EQUAL LOAD

### CONDITIONS FOR NO WARP

- o SEATS FOR LIVE LOAD SHOES AT PROPER ELEVATIONS
- o TRANSVERSE BALANCE
- O WARP ADJUSTMENT CLUTCH ADJUSTED

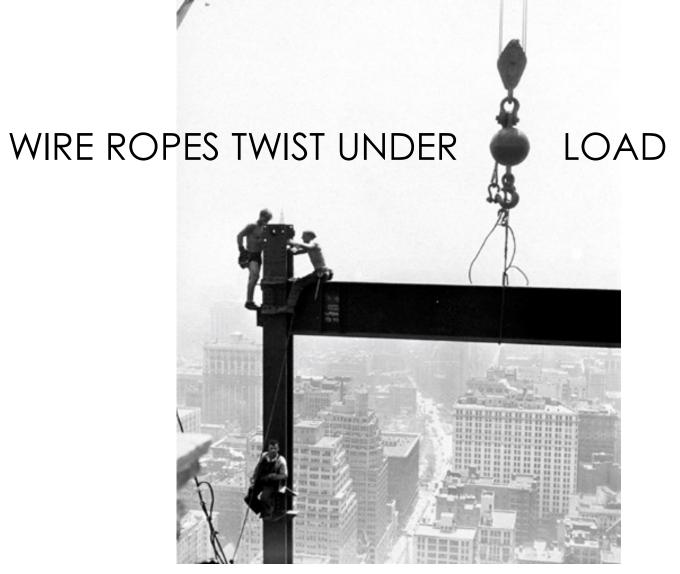
### INDICATORS OF WARP

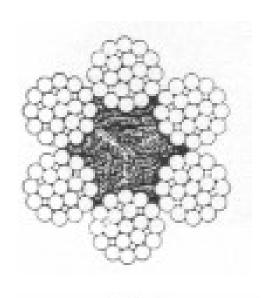
o ANOMOLIES IN BACKLASH

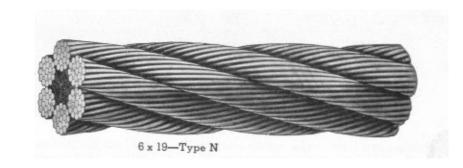
o A LIVE LOAD SHOE DOESN'T SEAT 

### OUTLINE

- o ANATOMY
- o ALIGNMENT OF COMPONENTS
- o DEFLECTIONS
- o SPAN ALIGNMENT
- ROPE LAY & CWT. TWIST

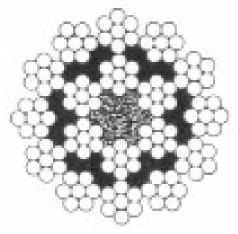






6 x 25 FIBER CORE

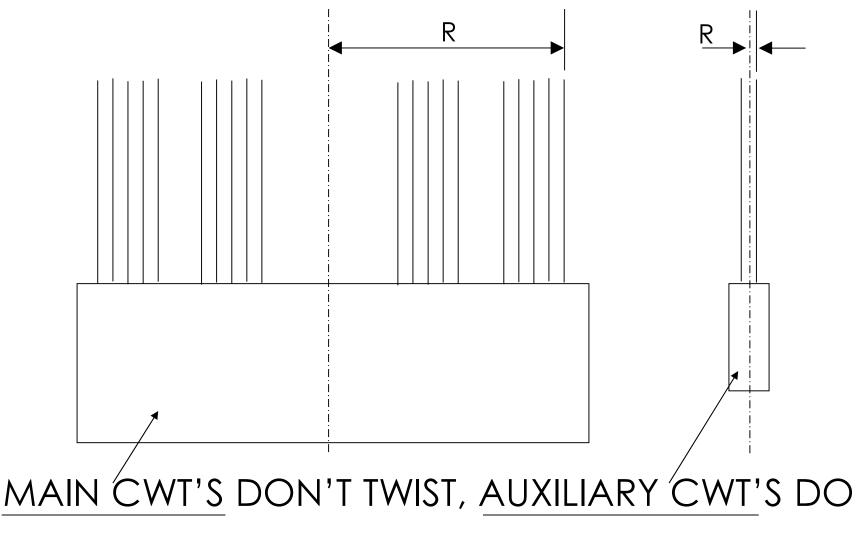
T=kDW

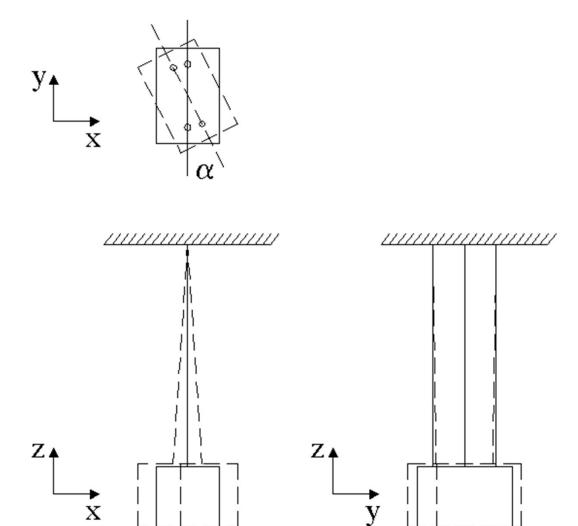




NON-TWISTING ROPE T=~0

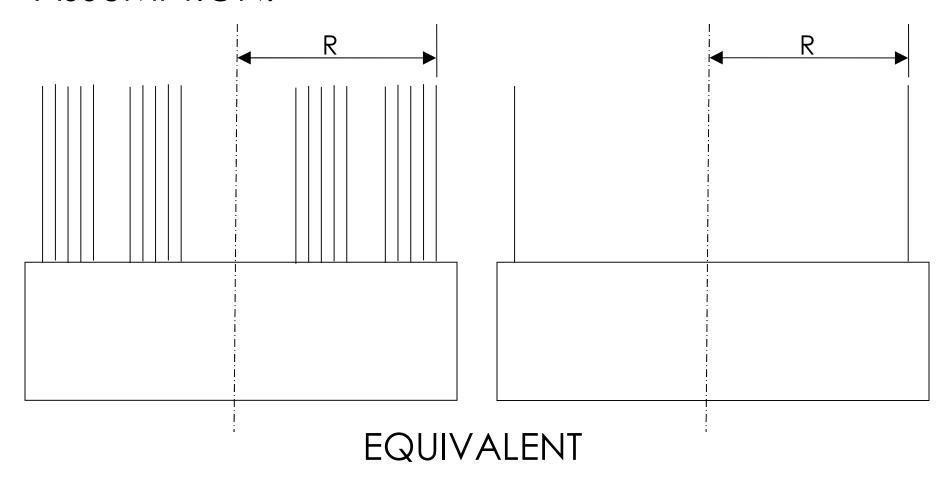
# ROPE LAY & COUTERWEIGHT TWIST EXPERIENCE SHOWS:





 $\uparrow \alpha \qquad \uparrow \text{ Weight}$   $\uparrow \alpha \qquad \uparrow \text{ Rope Diam}$   $\uparrow \alpha \qquad \uparrow \text{ Rope Free Length}$   $\downarrow \alpha \qquad \uparrow \text{ Dist Between Ropes}$ 

### **ASSUMPTION:**



### **ANALYSIS RESULTS:**

	MAIN CW	Л.	AUXILIARY CWT.		
WEIGHT	3 100 000	LB.	13 000	LB.	
ROPE DIAM	2 1/4	IN.	0.875	IN.	
ROPE TO CL (R)	450	IN.	3	IN.	
TORQUE	52 000	FT-LB	85	FT-LB	
TWIST ( $\alpha$ )	0.02°		+90°		



- o ANATOMY
- O ALIGNMENT OF COMPONENTS
- o DEFLECTIONS
- o SPAN ALIGNMENT
- o ROPE LAY & CWT. TWIST